

**PROCESS FOR THE PREPARATION OF LOW MOLECULAR  
WEIGHT HYDROGENATED NITRILE RUBBER**

**Field of the Invention**

5        The present invention relates to a process for the production of hydrogenated nitrile rubber polymers having lower molecular weights and narrower molecular weight distributions than those known in the art in the characterized that the process is carried out in the presence of hydrogen and optionally at least one co-(olefin).

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**Background of the Invention**

Hydrogenated nitrile rubber (HNBR), prepared by the selective hydrogenation of acrylonitrile-butadiene rubber (nitrile rubber; NBR, a copolymer comprising at least one conjugated diene, at least one unsaturated nitrile and optionally further co-monomers), is a specialty rubber which has very good heat resistance, excellent ozone and chemical resistance, and excellent oil resistance. Coupled with the high level of mechanical properties of the rubber (in particular the high resistance to abrasion) it is not surprising that HNBR has found widespread use in the automotive (seals, hoses, bearing pads) oil (stators, well head seals, valve plates), electrical (cable sheathing), mechanical engineering (wheels, rollers) and shipbuilding (pipe seals, couplings) industries, amongst others.

Commercially available HNBR has a Mooney viscosity in the range of from 55 to 105, a molecular weight in the range of from 200,000 to 500,000 g/mol, a polydispersity greater than 3.0 and a residual double bond (RDB) content in the range of from 1 to 18% (by IR spectroscopy).

One limitation in processing HNBR is the relatively high Mooney Viscosity. In principle, HNBR having a lower molecular weight and lower Mooney viscosity would have better processability. Attempts have been

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made to reduce the molecular weight of the polymer by mastication (mechanical breakdown) and by chemical means (for example, using strong acid), but such methods have the disadvantages that they result in the introduction of functional groups (such as carboxylic acid and ester groups) into the polymer, and the altering of the microstructure of the polymer. This results in disadvantageous changes in the properties of the polymer. In addition, these types of approaches, by their very nature, produce polymers having a broad molecular weight distribution.

A hydrogenated nitrile rubber having a low Mooney (<55) and improved processability, but which has the same microstructure as those rubbers which are currently available, is difficult to manufacture using current technologies. The hydrogenation of NBR to produce HNBR results in an increase in the Mooney viscosity of the raw polymer. This Mooney Increase Ratio (MIR) is generally around 2, depending upon the polymer grade, hydrogenation level and nature of the feedstock. Furthermore, limitations associated with the production of NBR itself dictate the low viscosity range for the HNBR feedstock. Currently, one of the lowest Mooney viscosity products available is Therban® VP KA 8837 (available from Bayer), which has a Mooney viscosity of 55 (ML 1+4 @ 20 100°C) and a RDB of 18%.

Co-pending applications PCT/CA02/00967, PCT/CA02/00966 and PCT/CA02/00965 disclose a process for the preparation of a, optionally hydrogenated, nitrile rubber comprising reacting a nitrile rubber in the presence of at least one co-olefin. Said co-pending applications disclose that the same catalyst may be used in the hydrogenation and the metathesis reaction. The present invention, however, discloses that the metathesis reaction may be conducted in the presence of hydrogen.

#### Summary of the Invention

We have now discovered that hydrogenated nitrile rubber having lower molecular weights and narrower molecular weight distributions than

those known in the art can be prepared by the metathesis of nitrile butadiene rubber in the presence of hydrogen and, optionally at least one co-(olefin). Thus, the inventive process is capable of producing a hydrogenated nitrile rubber having a molecular weight ( $M_w$ ) in the range of  
5 from 20,000 to 250,000, a Mooney viscosity (ML 1+4 @ 100 deg. C) of in the range of from 1 to 50, and a MWD (or polydispersity index) of less than 2.6 in a single step.

Description of the Invention

10 As used throughout this specification, the term "nitrile polymer" is intended to have a broad meaning and is meant to encompass a copolymer having repeating units derived from at least one conjugated diene, at least one alpha-beta-unsaturated nitrile and optionally further one or more co-polymerizable monomers.

15 The conjugated diene may be any known conjugated diene, in particular a C<sub>4</sub>-C<sub>6</sub> conjugated diene. Preferred conjugated dienes are butadiene, isoprene, piperylene, 2,3-dimethyl butadiene and mixtures thereof. Even more preferred C<sub>4</sub>-C<sub>6</sub> conjugated dienes are butadiene, isoprene and mixtures thereof. The most preferred C<sub>4</sub>-C<sub>6</sub> conjugated diene is butadiene.  
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The unsaturated alpha-beta-unsaturated nitrile may be any known alpha-beta-unsaturated nitrile, in particular a C<sub>3</sub>-C<sub>5</sub> alpha-beta-unsaturated nitrile. Preferred C<sub>3</sub>-C<sub>5</sub> alpha-beta-unsaturated nitriles are acrylonitrile, methacrylonitrile, ethacrylonitrile and mixtures thereof. The most preferred C<sub>3</sub>-C<sub>5</sub> α,β-unsaturated nitrile is acrylonitrile.  
25

30 Preferably, the copolymer comprises in the range of from 40 to 85 weight percent of repeating units derived from one or more conjugated dienes and in the range of from 15 to 60 weight percent of repeating units derived from one or more unsaturated nitriles. More preferably, the copolymer comprises in the range of from 60 to 75 weight percent of repeating units derived from one or more conjugated dienes and in the

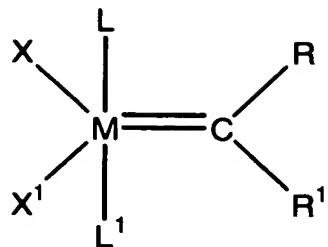
range of from 25 to 40 weight percent of repeating units derived from one or more unsaturated nitriles. Most preferably, the copolymer comprises in the range of from 60 to 70 weight percent of repeating units derived from one or more conjugated dienes and in the range of from 30 to 40 weight  
5 percent of repeating units derived from one or more unsaturated nitriles.

Optionally, the copolymer may further comprise repeating units derived from one or more co-polymerizable monomers, such as unsaturated carboxylic acids. Non-limiting examples of suitable unsaturated carboxylic acids are fumaric acid, maleic acid, acrylic acid,  
10 methacrylic acid and mixtures thereof. Repeating units derived from one or more co-polymerizable monomers will replace either the nitrile or the diene portion of the nitrile rubber and it will be apparent to the skilled in the art that the above mentioned figures will have to be adjusted to result in 100 weight percent. In case of the mentioned unsaturated carboxylic  
15 acids, the nitrile rubber preferably comprises repeating units derived from one or more unsaturated carboxylic acids in the range of from 1 to 10 weight percent of the rubber, with this amount displacing a corresponding amount of the conjugated diolefin. The presence of these co-monomers seems to enhance the metathesis reaction and allows conducting said  
20 reaction at temperatures in the range of from 0-50 °C.

Other preferred optionally further monomers are unsaturated mono- or di-carboxylic acids or derivatives thereof (e.g., esters, amides and the like) including mixtures thereof.

According to the invention the substrate is simultaneously subject  
25 to a metathesis reaction and a hydrogenation reaction.

The inventive process is conducted in the presence of one or more compounds of the general formula I,



Formula I

wherein

M is Os or Ru,

R and R<sup>1</sup> are, independently, hydrogen or a hydrocarbon selected  
5 from the group consisting of C<sub>2</sub>-C<sub>20</sub> alkenyl, C<sub>2</sub>-C<sub>20</sub> alkynyl, C<sub>1</sub>-C<sub>20</sub> alkyl,  
aryl, C<sub>1</sub>-C<sub>20</sub> carboxylate, C<sub>1</sub>-C<sub>20</sub> alkoxy, C<sub>2</sub>-C<sub>20</sub> alkenyloxy, C<sub>2</sub>-C<sub>20</sub>  
alkynyloxy, aryloxy, C<sub>2</sub>-C<sub>20</sub> alkoxy carbonyl, C<sub>1</sub>-C<sub>20</sub> alkylthio, C<sub>1</sub>-C<sub>20</sub>  
alkylsulfonyl and C<sub>1</sub>-C<sub>20</sub> alkylsulfinyl,

X and X<sup>1</sup> are independently any anionic ligand,

10 L is any neutral ligand, such as phosphines, amines, thioethers,

L' is an imidazolidinylidene or imidazolidine or any neutral carbone,  
optionally, L and L' can be linked to one another to form a bidentate  
neutral ligand;

Compounds of Formula I known as 2<sup>nd</sup> generation Grubb's  
15 catalysts, such as 1,3-bis-(2,4,6-trimethylphenyl)-2-imidazolidinylidene)-(tricyclohexylphosphine)ruthenium(phenylmethylene) dichloride are  
preferred.

The amount of catalytic compounds will depend upon the nature  
and catalytic activity of the compound(s) in question. Typically, the ratio of  
20 compound(s) to NBR is in the range of from 0.005 to 5, preferably in the  
range of from 0.025 to 1 and, more preferably, in the range of from 0.1 to  
0.5.

The process can be carried out in any suitable solvent which does  
not inactivate the catalyst or otherwise interfere with the reaction.

25 Preferred solvents include, but are not limited to, dichloromethane,

benzene, toluene, tetrahydrofuran, methyl ethyl ketone, cyclohexane and the like. The most preferred solvent is monochlorobenzene (MCB).

- The concentration of NBR in the reaction mixture is not critical but, obviously, should be such that the reaction is not hampered if the mixture
- 5 is too viscous to be stirred efficiently, for example. Preferably, the concentration of NBR is in the range of from 1 to 40% by weight, most preferably in the range of from 6 to 15 wt.%.

The concentration of hydrogen is usually between 500 psi and 2000 psi, preferably 1000 psi and 1400 psi.

- 10 The process is preferably carried out at a temperature in the range of from 0 to 140°C; preferably in the range of from 20 to 100°C.

The reaction time will depend upon a number of factors, including cement concentration, amount of catalyst used and the temperature at which the reaction is performed. The progress of the reaction may be

- 15 monitored by standard analytical techniques, for example using GPC or solution viscosity. Whenever referenced throughout the specification the molecular weight distribution of the polymer was determined by gel permeation chromatography (GPC) using a Waters 2690 Separation Module and a Waters 410 Differential Refractometer running Waters
- 20 Millenium software version 3.05.01. Samples were dissolved in tetrahydrofuran (THF) stabilized with 0.025% BHT. The columns used for the determination were three sequential mixed-B gel columns from Polymer Labs. Reference Standards used were polystyrene standards from American Polymer Standards Corp.

- 25 Hydrogenation in this invention is understood by preferably more than 50 % of the residual double bonds (RDB) present in the starting nitrile polymer being hydrogenated, preferably more than 90 % of the RDB are hydrogenated, more preferably more than 95 % of the RDB are hydrogenated and most preferably more than 99 % of the RDB are
- 30 hydrogenated.

The Mooney viscosity of the rubber can be determined using ASTM test D1646.

Due to the low viscosity of the resulting HNBR, it is ideally suited to be processed by but not limited to molding injection technology. The 5 polymer can also be useful to transfer molding, to compression molding, or to liquid injection molding.

Further, the inventive polymer is very well suited for the manufacture of a shaped article, such as a seal, hose, bearing pad, stator, well head seal, valve plate, cable sheathing, wheel, roller, pipe seal, in 10 place gaskets or footwear component prepared by injection molding technology.

### Examples

#### Examples 1-2

15 Tris(triphenylphosphine)Rhodium Chloride (Wilkinson's hydrogenation catalyst), 1,3-bis-(2,4,6-trimethylphenyl)-2-imidazolidinylidene) (tricyclohexylphosphine)- Ruthenium(phenylmethylene) dichloride (Grubbs 2<sup>nd</sup> generation metathesis catalyst). Triphenylphosphine (TPP) and monochlorobenzene 20 (MCB) were purchased from JMI, Materia Inc., Elf Atochem and PPG respectively and used as received.

The reactions were carried out in a 2 US gallon high pressure Parr Reactor under the following conditions:

25 Cement Concentration 12 wt.%  
Reaction Temperature see Table A  
Catalyst Type and Loading see Table A  
Solvent Monochlorobenzene  
Substrate Statistical Butadiene-acrylonitrile copolymer with 30 a acrylonitrile content of 34

wt% and a Mooney-Viscosity ML (1+4)@ 100 deg. C of 29 units.

	H <sub>2</sub> (g) pressure	1200 psi
5	Agitator Speed	600 rpm
	Reactor Temperature	138°C

The cement was degassed 3 times with H<sub>2</sub> (100 psi) under full agitation. The temperature of the reactor was raised to 130°C and a 60mL monochlorobenzene solution containing the catalyst and 10 triphenylphosphine (if needed) was added to the reactor. The temperature was allowed to increase to 138°C and maintained constant for the duration of the reaction. The hydrogenation reaction was monitored by measuring the residual double bond (RDB) level at various intervals using IR spectroscopy.

Example 1-2: Details**Table 1 Comparison of Hydrogenation Profiles**

Example 1			Example 2 (Comparative)	
Catalyst	Grubb's 2 <sup>nd</sup> Generation		Wilkinson's	
Catalyst loading	0.07 phr		0.07 phr	
Co-Catalyst	None		TPP, 1 phr	
Time	RDB (%)	ln(RDB)	RDB (%)	ln(RDB)
0	100	4.60	100	4.60
30			36.6	3.60
60	19.5	2.97	23.0	3.13
120	8.3	2.11	10.3	2.33
180	2	0.69	5.5	1.70
240	1.2	0.18	3.2	1.16

**Table 2 Summary of HNBR Properties**

	Mn	Mw	PDI
Example 1	66000	178000	2.70
Example 2	97000	314000	3.24

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Examples 3-4: Compounding and physical testing in Peroxide Recipe

Polymer composites were mixed on an open mill. The curatives were added on a cold open mill in a separate mixing step. The formulations used in this assessment are based on a simplified peroxide recipe.

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Carbon black N 660 Sterling-V available from Cabot Tire Blacks

Maglite® D is a MgO available from C.P. Hall.

Naugard® 445 is a diphenylamine available from Uniroyal Chemical.

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Plasthall TOTM is a Trioctyl trimellitate available from C.P. Hall.

Vulkanox® ZMB-2/C5 is a Zinc salt of 4- and 5-methyl-mercaptop benzimidazole available from Bayer AG

DIAK #7 is a Triallylisocyanurate available from DuPont Dow Elastomers

Vulcup 40KE is 2,2'-bis (tert-butylperoxy di-isopropylbenzene) available from Harwick Standard.

**Table 3 Peroxide Cure Compounding Recipe**

	Example 3	Example 4 (Comp.)
Polymer of Example 1	100	
THERBAN A 3406		100
CARBON BLACK, N 660 STERLING-V	50	50
MAGLITE D	3	3
NAUGARD 445	1	1
PLASTHALL TOTM	5	5
VULKANOX ZMB-2/C5 (ZMMBI)	0.4	0.4
ZINC OXIDE (KADOX 920) GRADE PC 216	3	3
DIAK #7	2	2
VULCUP 40KE	7	7

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**Polymer Composites Properties**

Table 4 shows a summary of the properties of polymer composites of Exp. 3 and 4. Example 4 is for comparison. The MDR cure characteristics were at 1.7 Hz, 1°arc, 180 °C, 30 min, 100 dNm.

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**Table 4 Summary of Polymer Composite Properties**

	Ex. 3	Ex. 4 (Comp)
<b>MOONEY VISCOSITY (ML1+4/100°C)</b>		
Raw Polymer	41.5	63.6
<b>COMPOUND MOONEY VISCOSITY (ML1+4/100°C)</b>		
Compound	58.6	77.4
MH (dN.m)	39.8	46.4
ML (dN.m)	1.5	2.2
Delta MH-ML (dN.m)	38.3	44.2
Modulus @ 100 (MPa)	4.8	6.3
Ultimate Tensile (MPa)	20.74	22.23
Ultimate Elongation (%)	254	247
Hardness Shore A2 (pts.)	61	63

From Table 4, it is clear that although the molecular weight (Mw) of the Low Mooney HNBR used in polymer composite 3 is only 66% of that of Therban® A3406, the physical properties remain very good.